Workshop II<br>MEEM-5650

Submitted by,
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## Executive Summary

This workshop focuses on identifying special causes affecting the operation that is used to manufacture a bronze bushing using statistical tools like control charts. It also encourages to take actions to eliminate these special causes and improving the process capability. For this, a sampling experiment is performed using TURSIM, an MS Excel based Visual Basic Program. This program simulates a single-point lathe turning operation to manufacture bronze bushing. The generated data is then analysed using control charts to identify the special causes affecting the process. After identifying these special causes and bring the process in statistical control process capability of the process is calculated. Further to improve the capability of the process corrective actions are taken.

The data generated shows the surface roughness on outside-diameter surface of the bronze bushing which is $70 \pm 15$ microinches specification. Ten potential special causes which may influence this process of manufacturing the bronze bushes are provided and out of these ten causes only three influence the surface roughness on outside-diameter surface of bronze bushing.

| Potential Special Causes | Levels of variation |
| :--- | :--- |
| Cutting Speed | 1000 to 1100 fpm |
| Feed Rate | 0.0080 to 0.0089 ipr |
| Setup Person | Samuel or Richard |
| Operator | Regura or Substitute |
| Tool Type | Nork-V, Cutgo-T, or Roved Cube |
| Tool Condition | Sharp or Dull |
| Depth-to-Shoulder | 0.0997 to 0.1003 inches |
| Machine | Nacirema, Rex or Le-Lathe |
| Measuring Device | Talymeas 5 or Surfchek 3 |
| Rake Angle | 5 or 10 Degrees |

The aim in this workshop is to identify these three special causes using $\bar{X}$ and $R$ control charts. This is done by analysing the chart by applying the Shewhart's control chart rules. The rule violation points are then analysed and correlation between the violated sample points and the given ten factors is seen. This provides the statistical signals which helps in identifying the special causes.

We have found that the three special causes that affect the surface roughness of the outsidediameter surface of bronze bushing are tool condition, operator and machine. The tool condition is changed to sharp and regular operator is used for the samples. For machine we have collected different data for each machine to avoid error of mixing. Le- Lathe and Nacirema machine show statistical control and process capability study is performed for them. Rex machine does not show process under statistical control and further this machine needs to be analysed for any other special cause.

## Introduction

In this workshop we have performed a sampling experiment using TURNSIM software, which generates data of a single point lathe turning operation used to manufacture a bronze bushing. The data generated is of a surface roughness of the outside diameter surface which is within specification $70 \pm 15$ microinches. In this generated data they are ten potential special causes given out of which only three influence the operation of manufacturing. The data has 5 subgroups with 40 sample size which is a decent number of samples to get accurate results. E We have used the MINITAB software to generate control charts, which provides statistical signals to identify the special causes. TURNSIM operates in a way where one special causes are identified then it removes that special cause.

## Procedure

The general procedure employed to complete this workshop is as, In the first run, TURNSIM generates data of surface roughness with subgroup size five and user specified samples size. We have generated forty samples for all the times we have collected data. Then the $\bar{X}$ and $R$ control charts are plot in MINITAB software and using statistical signals special causes are identified. When the first special cause is identified then while generating next data, TURNSIM ask's for identified special causes and entering them will disarm that causes if it is correct and generate the new data. This process is followed to identify all the three special causes. When these special causes are identified then for the controlled operation process capability study is performed. The values of percentage of products within specification, $\mathrm{C}_{\mathrm{p}}$ and $\mathrm{C}_{\mathrm{pk}}$ are found.

## Trial-1

Before starting our trial run we first narrowed down the parameters which could be the real potential cause for the increase in the roughness value, we eliminated the parameters that didn't have any relation with the surface roughness for example the Depth to shoulder ratio also the measuring instrument device which does not have any effect on the roughness value of the part machined. The cause and effect diagram helped in providing an overall mapping of all the parameters that could be a potential cause of the increase in surface roughness. We then simulated our first trial using TURNSIM software and plotted its $\overline{\mathrm{X}}$ and R control charts.


Cause and Effect Diagram for Surface Roughness


## Test Results for $\overline{\mathrm{X}}$ Chart for First Run

TEST 5.2 out of 3 points more than 2 standard deviations from centre line (on one side of CL). Test Failed at points: 30

## Test Results for R Chart for First Run

TEST 1. One point more than 3.00 standard deviations from centre line. Test Failed at points: $29,31,38$.

It can be seen from the R chart that there is a presence of special cause in the process and when the special causes are tracked back to the data sheet it was clear that the reason for the violation was due to the tool condition it is a clear indication from the scatter plot that the range of the surface roughness increases when the tool is blunt while the range remains low when the tool is sharp. Thus, tool condition might be the potential special cause.


## Trial - 2

For starting the second trail, the TURNSIM software takes input weather we have discovered any special cause in the process. As discussed earlier we have found that tool condition is a special cause in a process. Thus, we entered tool condition as identified special cause in a process and sample numbers equal to forty. The data generated then had only sharp tool condition and has eliminated the dull tool condition which led to source of special cause. Then we plotted the $\overline{\mathrm{X}}$ and R control charts for the new data generated and applied the Shewhart's control chart rules to search for violations and statistical signals.


Test Results for $\overline{\mathrm{X}}$ Chart for Second Run
TEST 1. One point more than 3.00 standard deviations from centre line. Test Failed at points: $45,50,53,56,74,76$
TEST 5.2 out of 3 points more than 2 standard deviations from centre line (on one side of CL). Test Failed at points: 45, 55, 76

Tracking the violations in the above chart to the potential causes we can see that the violation were when there was a substitute worker employed for the process. We can also see the evidence to this in the scatter plot. Thus, we came to conclusion that operator can be the second potential special cause which influence the surface roughness of the outside diameter surface of the bronze bushing.


## Trial-3

For the third trial as mentioned above we have to first feed the identified special causes and the TURNSIM then disarms those special causes. We selected tool condition and operator as special causes. The sample was kept same as forty. The new data generated had all tool to be sharp and the operator to be regular. We then plotted the $\overline{\mathrm{X}}$ and R control charts for the new data generated and applied the Shewhart's control chart rules to search for violations and statistical signals.


## Test Results for $\overline{\mathrm{X}}$ Chart for Third Run

TEST 1. One point more than 3.00 standard deviations from centre line. Test Failed at points: 82, 85, 118.
TEST 5.2 out of 3 points more than 2 standard deviations from centre line (on one side of CL). Test Failed at points: 85, 99, 100, 112.
TEST 6.4 out of 5 points more than 1 standard deviation from centre line (on one side of CL). Test Failed at points: 100.


From the rule violations in the $\overline{\mathrm{X}}$ and R control chart we checked the sample points in the data sheet to check for potential special cause. From the data sheet we could easily see that the violations were all at the Rex machine. Plotting and analysing the scatter plot we came to conclusion that machine would be the potential third special cause in the process which influence the surface roughness.

## Trial - 4

In the $4^{\text {th }}$ run of the TURNSIM, we have identified the three special causes which influence the process. We entered the three special causes: tool condition, operator and machine in the TURNSIM. We chose to keep the sample size same as forty. When we entered machine as a special cause the TURNSIM asked us weather we want data to be in group of different machine or a mix of data from all machine. To avoid the error of mixing we chose the data to be different. The new data generated was of forty sample size of data for each machine. We then plotted the $\overline{\mathrm{X}}$ and R control chart for check weather the potential special causes selected are accurate. From the $\overline{\mathrm{X}}$ and R control chart below we can see that there are no rule violation for the Le-Lathe and Nacirema machine and thus the special causes identified are correct as the process is under statistical control. We could see that for Rex machine there is rule violation in the R chart thus there are still special causes in the Rex machine process which are needed to be identified.




Test Results for R Chart for Rex Machine
TEST 2.8 points in a row on same side of centre line. Test Failed at points: 228, 229.

## Conclusion

The special causes identified in this workshop are the tool condition, operator and machine. The tool condition is changed to sharp and regular operator is used for the samples. For machine we have collected different data for each machine to avoid error of mixing. Le- Lathe and Nacirema machine show statistical control and process capability study is performed for them. The Rex machine is not under statistical control and we have seen that from the start that Rex machine is the source of special cause. The Rex machine shows violation at sample number 228 and 229. Thus, we can say that further identification of special causes is required for the Rex machine.

From the above we can conclude that to avoid special causes to come in the process, sharp tool should be used and regular operator should be employed instead of substitute operator to bring the surface roughness value of the outside diameter surface on bronze bushing close to nominal value.

The process capability study is performed for the Nacirema and Le-Lathe machine. The values of $\mathrm{C}_{\mathrm{p}}$ and $\mathrm{C}_{\mathrm{pk}}$ are less than 1 and percent of surface roughness are also less than $99.73 \%$. Thus, we can say that the process of manufacturing of bronze bushing is not capable.

To increase the process capability of the Nacirema and Le-Lathe machine the surface roughness value should be brought as close to the nominal value of 70 microinches. It could be done by finding the common causes affecting the process and eliminating them. This would bring fundamental change to the process capability. For the Rex machine further statistical study is required to search and eliminate the special causes to bring process under statistical control.

## Process Capability

1. Process capability study for process running on Le-lathe machine:
2. $C_{\mathrm{p}}=\frac{(\mathrm{USL}-\mathrm{LSL})}{6 * \sigma}$

As from the control charts,
$\overline{\mathrm{R}}=16.23, \mu=62.73$
For $\mathrm{n}=5, \mathrm{~d}, \mathrm{~d}_{2}=2.326$
$\sigma=\overline{\mathrm{R}} / \mathrm{d}_{2}=16.23 / 2.326=6.98$
$C_{\mathrm{p}}=\frac{(\mathrm{USL}-\mathrm{LSL})}{6 * \sigma}$
$C_{\mathrm{p}}=\frac{(85-55)}{6 * 6.98}$
$C_{\mathrm{p}}=0.72$
2. For calculating $C_{\mathrm{pk}}$,
$Z_{\text {USL }}=(\mathrm{USL}-\mu) / \sigma$
$Z_{\text {USL }}=(85-62.73) / 6.98=3.19$
$\mathrm{Z}_{\mathrm{LSL}}=(\mathrm{LSL}-\mu) / \sigma$
$\mathrm{Z}_{\mathrm{LSL}}=(55-65.45) / 7.46=-1.107$
$\mathrm{Z}_{\text {min }}=\min \left[Z_{\mathrm{USL},}, \mathrm{Z}_{\mathrm{LSL}}\right]$
$Z_{\text {min }}=-(-1.107)=1.107$
$C_{\mathrm{pk}}=\frac{Z_{\text {min }}}{3}=0.37$
Capability Index
$C_{\mathrm{p}}=0.72$
$C_{\mathrm{pk}}=0.37$
3. Products having surface roughness within specifications:

Area within specifications is $0.9992-0.1341=0.8651$
\% of products within specifications is 86.51

## 2. Process capability study for process running on Nacirema machine:

1. $C_{\mathrm{p}}=\frac{(\mathrm{USL}-\mathrm{LSL})}{6 * \sigma}$

As from the control charts,
$\overline{\mathrm{R}}=16.7, \mu=76.83$
For $\mathrm{n}=5, \mathrm{~d}, \mathrm{~d}_{2}=2.326$
$\sigma=\overline{\mathrm{R}} / \mathrm{d}_{2}=16.7 / 2.326=7.18$
$C_{\mathrm{p}}=(\mathrm{USL}-\mathrm{LSL}) / 6^{*} \sigma$
$C_{\mathrm{p}}=\frac{(85-55)}{6 * 7.18}$
$C_{\mathrm{p}}=0.696$
2. For calculating Cpk,
$Z_{\text {USL }}=(\mathrm{USL}-\mu) / \sigma$
$Z_{\text {USL }}=(85-76.83) / 7.18=1.13$
$\mathrm{Z}_{\mathrm{LSL}}=(\mathrm{LSL}-\mu) / \sigma$
$Z_{\mathrm{LSL}}=(55-76.83) / 7.18=-3.04$
$\mathrm{Z}_{\text {min }}=\min \left[\mathrm{Z}_{\mathrm{USL}},-\mathrm{Z}_{\mathrm{LSL}}\right]$
$\mathrm{Z}_{\text {min }}=1.13$
$C_{\mathrm{pk}}=\frac{Z_{\min }}{3}=0.376$

Capability Index
$C_{\mathrm{p}} 0.696$
$C_{\mathrm{pk}}=0.376$
3. Products having surface roughness within specifications:

Area within specifications is $0.8707-0.001183=0.8695$
\% of products within specifications is 86.95
3. Process running on Rex machine:

After observing R chart plotted for Rex machine it is inferred that process is not under statistical control as two points in that plot (Point 228 and 229) violates Shewhart's chart test rules for R chart. Hence, we are not evaluating process capability for this machine.

## Appendix:

Trial 1:

| Name | Group No-7 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Date | 11-23-2019 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Instructor | Dr. Radheshya | $m$ Tewari |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| TA | Mr. Salil Sule |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Trial | 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Subgroup: | 40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Special Caus | ause |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | Candidate Spe | cial Causes of Var | ariation and The | ir Levels |  |  |  |  |  |  |  |  | mple Rou | hness (m | oinches) |  |  |
| Test No. | Cutting Speed | Feed Rate (ipr) | Set up Person | Operator | Tool Type | Tool Condition | Depth-to-Shoulder | Machine | Measuring Device | Rake Angle (deg.) | 1 | 2 | 3 | 4 | 5 | X bar | R |
| 1 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 86.416 | 79.902 | 67.286 | 72.552 | 68.234 | 74.878 | 19.13 |
| 2 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 66.997 | 63.85 | 63.677 | 80.739 | 73.167 | 69.686 | 17.062 |
| 3 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 68.774 | 81.587 | 59.692 | 73.499 | 59.229 | 68.5562 | 22.358 |
| 4 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-v | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 57.596 | 67.237 | 63.116 | 62.234 | 58.608 | 61.7582 | 9.641 |
| 5 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 79.209 | 67.185 | 75.043 | 83.31 | 60.387 | 73.0268 | 22.923 |
| 6 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-v | Sharp | 0.0997 | Le-Lathe | Talymeas 5 | 5 | 62.61 | 62.596 | 67.769 | 55.682 | 56.604 | 61.0522 | 12.087 |
| 7 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 77.092 | 74.598 | 66.538 | 71.994 | 83.454 | 74.7352 | 16.916 |
| 8 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 72.716 | 70.731 | 74.265 | 67.069 | 70.196 | 70.9954 | 7.196 |
| 9 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 68.429 | 70.128 | 64.569 | 60.354 | 63.058 | 65.3076 | 9.774 |
| 10 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.0997 | Rex | Surfchek 3 | 10 | 55.225 | 60.937 | 72.156 | 74.841 | 77.044 | 68.0406 | 21.819 |
| 11 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 52.458 | 66.3 | 62.912 | 65.059 | 78.649 | 65.0756 | 26.191 |
| 12 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.1 | Rex | Surfchek 3 | 10 | 58.715 | 79.903 | 85.204 | 49.665 | 60.418 | 66.781 | 35.539 |
| 13 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 68.539 | 63.623 | 81.3 | 72.307 | 80.264 | 73.2066 | 17.677 |
| 14 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 69.234 | 82.154 | 68.609 | 84.033 | 87.741 | 78.3542 | 19.132 |
| 15 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 60.255 | 66.292 | 63.61 | 70.582 | 72.938 | 66.7354 | 12.683 |
| 16 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 63.277 | 55.719 | 76.8 | 72.642 | 55.626 | 64.8128 | 21.174 |
| 17 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 77.311 | 65.591 | 56.491 | 64.316 | 72.957 | 67.3332 | 20.82 |
| 18 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 69.252 | 69.887 | 61.765 | 70.12 | 67.217 | 67.6482 | 8.355 |
| 19 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 69.748 | 57.052 | 64.249 | 64.508 | 63.707 | 63.8528 | 12.696 |
| 20 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 58.772 | 63.728 | 66.804 | 79.275 | 62.463 | 66.2084 | 20.503 |
| 21 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 61.742 | 63.019 | 72.507 | 68.24 | 58.314 | 64.7644 | 14.193 |
| 22 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 65.904 | 83.546 | 72.232 | 73.087 | 59.434 | 70.8406 | 24.112 |
| 23 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 82.599 | 66.789 | 62.559 | 79.597 | 66.875 | 71.6838 | 20.04 |
| 24 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 71.256 | 60.81 | 64.022 | 68.911 | 84.218 | 69.8434 | 23.408 |
| 25 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 67.26 | 76.173 | 62.907 | 72.762 | 63.025 | 68.4254 | 13.266 |
| 26 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 57.582 | 64.564 | 58.332 | 66.641 | 60.982 | 61.6202 | 9.059 |
| 27 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 71.617 | 70.29 | 74.522 | 59.56 | 70.689 | 69.3356 | 14.962 |
| 28 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 83.411 | 63.468 | 75.859 | 74.077 | 88.087 | 76.9804 | 24.619 |
| 29 | 1050 | 0.0089 | Mr. Ricard | Substitute | Nork-V | Dull | 0.1003 | Rex | Surfchek 3 | 10 | 71.686 | 76.384 | 49.665 | 58.616 | 98.792 | 71.0286 | 49.127 |
| 30 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 78.7 | 79.121 | 77.94 | 82.947 | 73.262 | 78.394 | 9.685 |
| 31 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.0997 | Rex | Surfchek 3 | 10 | 74.683 | 25.86 | 68.583 | 68.066 | 80.375 | 63.5134 | 54.515 |
| 32 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.0997 | Rex | Surfchek 3 | 10 | 82.946 | 72.817 | 51.214 | 74.286 | 59.199 | 68.0924 | 31.732 |
| 33 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 53.299 | 71.045 | 59.013 | 52.652 | 72.051 | 61.612 | 19.399 |
| 34 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 63.681 | 56.766 | 56.041 | 72.299 | 72.391 | 64.2356 | 16.35 |
| 35 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 70.176 | 74.758 | 66.174 | 73.084 | 65.731 | 69.9846 | 9.027 |
| 36 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.0997 | Rex | Surfchek 3 | 10 | 66.909 | 75.395 | 56.583 | 53.964 | 43.578 | 59.2858 | 31.817 |
| 37 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 70.395 | 82.292 | 72.634 | 77.365 | 82.878 | 77.1128 | 12.483 |
| 38 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Dull | 0.1 | Rex | Surfchek 3 | 10 | 45.539 | 70.41 | 71.082 | 115.395 | 41.167 | 68.7186 | 74.228 |
| 39 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 70.028 | 62.937 | 46.322 | 60.478 | 73.709 | $62.6948{ }^{\prime \prime}$ | 27.387 |
| 40 | 1100 | 0.008 | Mr. Samue | Regular | Nork-v | Sharp | 0.0997 | Le-Lathe | Talymeas 5 | 5 | 61.233 | 64.044 | 60.32 | 73.316 | 70.309 | 65.8444 | 12.996 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Trial 2:

| Date | 11/27/2019 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trial | 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Subgroup: | 40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Special CaTool Condition |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Test No. | Candidate Special Causes of Variation and Their Levels |  |  |  |  |  |  |  |  |  | Sample Roughness (microinches) |  |  |  |  |  |  |
|  | Cutting Speed | Feed Rate (ipr) | Set up Person | Operator | Tool Type | Tool Condition | Depth-to-Shoulder | Machine | Measuring Device | Rake Angle (deg.) | 1 | 2 | , | 4 | 5 | X bar | R |
| 41 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 79.522 | 73.528 | 60.531 | 79.069 | 74.182 | 73.3664 | 18.991 |
| 42 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 64.043 | 57.357 | 57.172 | 73.788 | 60.884 | 62.6488 | 16.616 |
| 43 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 82.219 | 95.048 | 63.622 | 89.457 | 62.471 | 78.5634 | 32.577 |
| 44 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 59.741 | 80.303 | 78.802 | 77.052 | 72.903 | 73.7602 | 20.562 |
| 45 | 1050 | 0.0089 | Mr. Ricard | tute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 89.477 | 67.423 | 71.086 | 89.658 | 98.867 | 83.3022 | 31.444 |
| 46 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 75.598 | 77.761 | 89.604 | 66.422 | 64.031 | 74.6832 | 25.573 |
| 47 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 82.078 | 77.487 | 68.653 | 74.192 | 60.437 | 72.5694 | 21.641 |
| 48 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 82.917 | 77.503 | 66.867 | 80.659 | 61.399 | 73.869 | 21.518 |
| 49 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 63.621 | 65.316 | 60.048 | 56.786 | 58.394 | 60.833 | 8.53 |
| 50 | 1050 | 0.0089 | Mr. Ricard | , | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 73.707 | 73.181 | 84.578 | 87.818 | 90.759 | 82.0086 | 17.578 |
| 51 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 72.313 | 77.622 | 67.804 | 82.278 | 75.415 | 75.0864 | 14.474 |
| 52 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 66.277 | 77.142 | 80.557 | 64.141 | 68.23 | 71.2694 | 16.416 |
| 53 | 1050 | 0.0089 | Mr. Ricard | ubstitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 63.557 | 97.931 | 91.465 | 72.043 | 88.739 | 82.747 | 34.374 |
| 54 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 74.592 | 58.328 | 73.837 | 62.504 | 66.395 | 67.1312 | 16.264 |
| 55 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 71.539 | 79.23 | 75.078 | 86.065 | 83.603 | 79.103 | 14.526 |
| 56 | 1100 | 0.008 | Mr. Samuel | Substitute | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 63.761 | 57.102 | 47.735 | 74.616 | 57.028 | 60.0484 | 26.881 |
| 57 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 78.801 | 66.493 | 59.702 | 68.928 | 78.752 | 70.5352 | 19.099 |
| 58 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 75.473 | 76.739 | 61.322 | 77.206 | 78.692 | 73.8864 | 17.37 |
| 59 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 81.55 | 67.12 | 73.76 | 74.139 | 79.62 | 75.2378 | 14.43 |
| 60 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 66.251 | 70.419 | 73.331 | 86.594 | $69.715^{\prime \prime}$ | 73.262' | 20.343 |
| 61 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 67.014 | 62.397 | 63.347 | 60.382 | $69.483^{\prime \prime}$ | 64.5246" | 9.101 |
| 62 | 100 | . 08 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 61.96 | 54.148 | 68.315 | 69.323 | 55.392' | 61.8276" | 15.17 |
| 63 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 79.033 | 86.579 | 83.818 | 76.647 | $81.787^{\prime \prime}$ | 81.5728' | 9.932 |
| 64 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 69.831 | 54.576 | 67.584 | 71.894 | $62.664^{\prime}$ | 65.3098' | 17.318 |
| 65 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 59.326 | 70.474 | 77.931 | 67.665 | $78.067^{\prime \prime}$ | 70.6926 ${ }^{\prime}$ | 18.741 |
| 66 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 70.768 | 57.743 | 71.646 | 60.341 | 79.539 | 68.0074 ${ }^{\prime \prime}$ | 21.796 |
| 67 | 100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 68.939 | 67.372 | 73.355 | 57.432 | $63.269^{\prime \prime}$ | $66.0734^{\prime \prime}$ | 15.923 |
| 68 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 70.963 | 74.424 | 63.895 | 60.674 | 72.839' | 68.559' | 13.7 |
| 69 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 76.404 | 82.72 | 70.141 | 73.443 | $68.879^{\prime}$ | 74.3174' | 13.84 |
| 70 | 1050 | 0.0089 | Mr. Ricard | Substitute | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 79.872 | 80.263 | 79.099 | 82.694 | 78.908 | 80.1672' | 3.786 |
| 71 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 76.421 | 83.015 | 73.437 | 73.159 | 78.738' | 76.954 ${ }^{\prime}$ | 9.856 |
| 72 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 82.529 | 74.519 | 64.627 | 75.391 | 67.694' | 72.952' | 17.902 |
| 73 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 80.185 | 73.81 | 61.112 | 61.766 | 81.015' | 71.5776' | 19.903 |
| 74 | 1100 | 0.008 | Mr. Samuel | ubstitute | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 65.685 | 59.582 | 59.439 | 48.122 | 48.667 ${ }^{\prime \prime}$ | 56.299' | 17.563 |
| 75 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 76.584 | 59.572 | 71.934 | 85.532 | 71.548' | 73.034", | 25.96 |
| 76 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-v | Sharp | 0.0997 | Le-Lathe | Talymeas 5 | 5 | 53.529 | 60.324 | 53.741 | 63.553 | 61.436 ${ }^{\prime}$ | 58.5166" | 10.024 |
| 77 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 77.589 | 62.591 | 79.954 | 85.878 | $63.257^{\prime \prime}$ | 73.8538" | 23.287 |
| 78 | 1050 | 0.0089 | Mr. Ricard | Substitute | Nork-V | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 68.999 | 80.854 | 81.56 | 55.009 | 57.643" | 68.813' | 26.551 |
| 79 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 73.773 | 64.931 | 55.741 | 61.46 | 79.106" | 67.0022' | 23.365 |
| 80 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 66.941 | 70.381 | 66.066 | 58.71 | $56.207^{\prime \prime}$ | 63.661 | 14.174 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Trial 3:

| Date | 11/27/2019 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trial | 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Subgroup: | 40 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Special Ca Operator,Tool Condition, |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Test No. | Candidate Special Causes of Variation and Their Levels |  |  |  |  |  |  |  |  |  | Sample Roughness (microinches) |  |  |  |  |  |  |
|  | Cutting Speed | Feed Rate (ipr) | Set up Person | Operator | Tool Type | Tool Condition | Depth-to-Shoulder | Machine | Measuring Device | Rake Angle (deg.) | 1 | 2 | 3 | 4 | 5 | x bar | R |
| 81 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 77.601 | 73.68 | 81.066 | 77.409 | 74.267 | 76.8046 | 7.386 |
| 82 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 72.886 | 95.294 | 92.402 | 80.607 | 80.728 | 84.3834 | 22.408 |
| 83 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-v | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 59.264 | 63.841 | 69.082 | 62.399 | 68.606 | 64.6384 | 9.818 |
| 84 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 74.914 | 65.423 | 56.652 | 84.221 | 77.607 | 71.7634 | 27.569 |
| 85 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Rex | Talymeas 5 | 5 | 67.251 | 55.66 | 64.657 | 47.698 | 63.195 | 59.6922 | 19.553 |
| 86 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 71.841 | 57.708 | 66.802 | 74.426 | 75.044 | 69.1642 | 17.336 |
| 87 | 1050 | 0.0089 | Mr. Ricard | Regular | Nork-V | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 74.302 | 72.41 | 83.889 | 69.37 | 76.568 | 75.3078 | 14.519 |
| 88 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 80.707 | 78.508 | 74.89 | 64.192 | 70.578 | 73.775 | 16.515 |
| 89 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 63.411 | 65.103 | 59.799 | 67.376 | 70.516 | 65.241 | 10.717 |
| 90 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1001 | Nacirema | Talymeas 5 | 5 | 77.669 | 77.215 | 62.993 | 64.808 | 65.973 | 69.7316 | 14.676 |
| 91 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 55.96 | 62.547 | 59.813 | 77.082 | 66.152 | 64.3108 | 21.122 |
| 92 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 74.083 | 86.936 | 62.722 | 72.248 | 75.91 | 74.3798 | 24.214 |
| 93 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 72.233 | 67.852 | 67.953 | 79.316 | 67.079 | 70.8866 | 12.237 |
| 94 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 66.629 | 82.135 | 66.201 | 55.979 | 61.085 | 66.4058 | 26.156 |
| 95 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 67.75 | 71.596 | 69.52 | 76.547 | 75.119 | 72.1064 | 8.797 |
| 96 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 57.378 | 66.596 | 63.869 | 62.546 | 66.548 | 63.3874 | 9.218 |
| 97 | 1050 | 0.0089 | Mr. Ricard | Regular | Nork-V | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 75.291 | 83.958 | 78.409 | 73.085 | 81.738 | 78.4962 | 10.873 |
| 98 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 77.603 | 78.261 | 71.341 | 78.508 | 80.594 | 77.2614 | 9.253 |
| 99 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 65.757 | 79.284 | 83.377 | 83.712 | 82.753 | 78.9766 | 17.955 |
| 100 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 78.571 | 81.267 | 85.514 | 75.936 | 80.636 | 80.3848 | 9.578 |
| 101 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 64.021 | 65.268 | 72.729 | 68.366 | 58.458 | 65.7684 | 14.271 |
| 102 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 79.368 | 71.844 | 65.398 | 66.345 | 73.59 | 71.309 | 13.97 |
| 103 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 64.685 | 70.044 | 68.489 | 62.375 | 67.025 | 66.5236 | 7.669 |
| 104 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 67.291 | 58.215 | 61.65 | 74.942 | 63.679 | 65.1554 | 16.727 |
| 105 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1 | Rex | Surfchek 3 | 10 | 80.522 | 70.213 | 76.855 | 64.248 | 76.927 | 73.753 | 16.274 |
| 106 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 85.83 | 71.76 | 87.47 | 73.995 | 65.847 | 76.9804 | 21.623 |
| 107 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 77.375 | 75.386 | 51.125 | 66.932 | 72.045 | 68.5726 | 26.25 |
| 108 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 65.021 | 81.543 | 71.079 | 68.464 | 79.812 | 73.1838 | 16.522 |
| 109 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 77.331 | 79.609 | 65.496 | 70.663 | 61.619 | 70.9436 | 17.99 |
| 110 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 65.062 | 65.657 | 63.556 | 68.242 | 83.12 | 69.1274 | 19.564 |
| 111 | 1050 | 0.0089 | Mr. Ricard | Regular | Nork-V | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 75.048 | 81.029 | 71.9 | 78.483 | 87.406 | 78.7732 | 15.506 |
| 112 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.0997 | Rex | Surfchek 3 | 10 | 65.945 | 85.615 | 74.152 | 87.788 | 76.799 | 78.0598 | 21.843 |
| 113 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 72.081 | 68.166 | 75.69 | 71.886 | 68.742 | 71.313 | 7.524 |
| 114 | 1050 | 0.0089 | Mr. Ricard | Regular | Roved Cube | Sharp | 0.1003 | Rex | Surfchek 3 | 10 | 69.128 | 82.735 | 82.552 | 77.408 | 77.454 | 77.855 | 13.607 |
| 115 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0998 | Le-Lathe | Talymeas 5 | 5 | 70.295 | 52.959 | 65.739 | 77.837 | 69.474 | 67.2608 | 24.878 |
| 116 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0999 | Le-Lathe | Talymeas 5 | 5 | 65.604 | 70.489 | 55.671 | 53.548 | $75.527^{\prime}$ | $64.1678^{\prime \prime}$ | 21.979 |
| 117 | 1000 | 0.0086 | Mr. Samuel | Regular | Cutgo-T | Sharp | 0.1 | Nacirema | Talymeas 5 | 5 | 71.343 | 54.617 | 73.675 | 79.265 | 55.713 | 66.9226' | 24.648 |
| 118 | 1050 | 0.0089 | Mr. Ricard | Regular | Nork-V | Sharp | 0.1003 | Le-Lathe | Surfchek 3 | 10 | 78.476 | 88.71 | 91.021 | 74.165 | 74.669 | $81.4082^{\prime \prime}$ | 16.856 |
| 119 | 1000 | 0.0086 | Mr. Ricard | Regular | Cutgo-T | Sharp | 0.1002 | Nacirema | Surfchek 3 | 10 | 66.919 | 82.609 | 70.532 | 66.167 | $79.749^{\prime \prime}$ | $73.1952^{\prime \prime}$ | 16.442 |
| 120 | 1100 | 0.008 | Mr. Samuel | Regular | Nork-V | Sharp | 0.0997 | Le-Lathe | Talymeas 5 | 5 | 67.235 | 70.796 | 66.346 | 59.058 | $56.684^{\prime \prime}$ | 64.0238 | 14.112 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



